

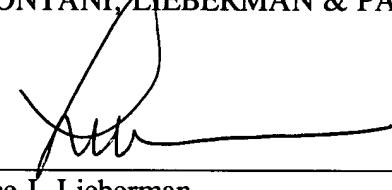
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**REMARKS**

This preliminary amendment is presented to place the application in proper form for examination and to eliminate multiple dependency from the present claims. No new matter has been added. Early examination and favorable consideration of the above-identified application is earnestly solicited.

Any additional fees or charges required at this time in connection with the application may be charged to our Patent and Trademark Office Deposit Account No. 03-2412.

Respectfully submitted,  
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*MPR/S*  
By Express Mail # EL503712193US · February 22, 2002**AMENDMENTS TO THE SPECIFICATION AND CLAIMS SHOWING CHANGES****In the Specification:**

On page 1, line 2, delete "Description" and insert the following headings:

**--BACKGROUND OF THE INVENTION****1. Field of the Invention--**

On page 1, amend the paragraph beginning on line 3 as follows:

--This invention [concerns] relates to a twin-screw extruder [according to the main concept of patent claim 1] with a cylinder surrounding the twin-screws of the extruder and a hollow cylinder mantle surrounding the cylinder.--

On page 1, before line 5, beginning a new line insert the following heading:

**2. Description of the Prior Art--**

On page 2, amend the paragraph beginning on line 24 as follows:

--Another structure for the cylinder of a twin-screw extruder is known from DE 26 59 037 C3, which likewise consists of an inner cylinder part and a hollow-cylinder mantle. For cooling of the extrusion space, a cooling channel is provided that has a course similar in principle to a [screw line] helix. The cooling channel is arranged in the region of the surface separating the inner cylinder part and the hollow-cylinder mantle. In this case it is composed of partial pieces of different shapes, in the following manner: on the upper side of the inner cylinder

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part, grooves are etched at equal distances from one another, with vertical walls, in such a way that the bottoms of the grooves are all parallel to the longitudinal axes of the planes in the twin-screw unit, the direction with respect to the longitudinal axis is chosen, however, at exactly the opposite angle. The arrangement of the upper and lower grooves and their distances are selected in such a way that their ends overlap pair-wise. In order to connect the overlapping ends in view of joining the tempering media, sickle-shaped connecting grooves are etched on the inner surface of the hollow-cylinder mantle. The cooling channels generated in this manner, which run like [screw lines] helices, have the advantage that the tempering medium in the region of the spandrel of the spectacle-shaped hole is brought to the extrusion space relatively densely. From the viewpoint of manufacturing technology, creating of the cooling channel still requires a comparably high expense, since not only must the grooves be etched on the upper and lower side of the inner cylinder part, but etching work is also necessary on the inner side of the hollow-cylinder mantle. In addition, the hollow-cylinder mantle produced in this way is only usable for the corresponding inner cylinder part of a twin-screw extruder, but not as an inner cylinder part for a single-screw extruder.--

On page 4, amend the paragraph beginning on line 6 as follows:

--Another solution for a cylinder of a twin-screw extruder that has an inner cylinder part and a hollow-cylinder mantle surrounding it is known from DE-OS 20 61 700, which is the overall state of the art. The wall of the inner cylinder part is cut through with numerous adjacent grooves above, below, and to the side of the spectacle-shaped hole for the

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twin-screw unit. The bottoms of these grooves run in straight-line segments or in arcs in such a way that the remaining wall to the extrusion space has approximately the same thickness everywhere. This requires a correspondingly high manufacturing cost. In order for connect the individual grooves into a channel running like a [screw line] helix for the cooling medium, the grooves on the bottom side of the inner cylinder part are connected together in such a way that three partial pieces, two of which run perpendicular to the longitudinal axis of the twin-screw unit and a middle one is directed at an angle to the longitudinal axis, in such a way that an overflow from one winding of the cooling channel to the next results. This in turn leads to an increase in manufacturing costs for the inner cylinder part. Since walls (bridges) remaining between the individual windings of the cooling channel should serve to transfer loads to the hollow-cylinder mantle that surrounds the inner cylinder part, the bridges, which have relatively small dimensions, arranged above and below the spectacle-shaped hole of the extrusion space and were originally especially high, are etched on a surface parallel to the plane of the twin-screw unit. On this etched surface, the bridges are each made in a cylinder section formed from filling material on the upper side and on the lower side of the inner cylinder part, the outer contour of the cylinder section corresponding to the hollow-cylinder mantle. These cylinder sections cover the individual windings of the cooling channels from top to bottom. In this way, the cross-section of the cooling channel, when viewed from above the circumference, remains approximately uniform in size. Although this known construction makes it possible to use a hollow-cylinder mantle with a smooth inner surface, it not only requires an increased manufacturing cost to generate the individual winding of the cooling channel, but also an additional cost for creating the two cylinder segments.--

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On page 5, after line 20, beginning its own line insert the following heading:

**--SUMMARY OF THE PRESENT INVENTION--**

On page 5, amend the paragraph beginning on line 21 as follows:

--The [task] object of the present invention is to develop a cylinder [according to the overall concept of patent claim 1] for a twin-screw extruder so that the manufacturing cost required remains as small as possible, whereby an especially uniform and effective tempering of the extrusion space is to be provided. In addition, the hollow-cylinder mantle of the cylinder should be usable universally, as far as possible. Specifically, it should be usable for single-screw as well as twin-screw extruders.--

On page 6, delete lines 5-7 in their entirety and insert the following therefore:

--The object of the present invention is met by a cylinder assembly for a twin-screw extruder having a cylinder with a variable wall thickness which defines an extrusion space for receiving twin screws of the twin-screw extruder. A hollow-cylinder mantle surrounds the cylinder. At least one channel having a helical shape and a cycle depth is formed on an outer side of the cylinder by a winding vortex process. An inlet and outlet are formed in the hollow-cylinder mantle in communication with the at least one channel for allowing a flow of a tempering medium from the inlet to the outlet via the at least one channel. The hollow-cylinder mantle closes the at least one channel. The cycle depth of the at least one channel varies along

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the circumferential direction of the cylinder such that the cycle depth is largest in regions where the wall thickness of the cylinder is largest and the cycle depth is smallest in regions where the wall thickness of the cylinder is smallest.--

On page 6, amend the paragraph beginning on line 8 as follows:

--The present invention starts from a twin-screw extruder with a cylinder, which surrounds the twin-screw of the extruder, forming an extrusion space. The cylinder is surrounded in turn by a hollow-cylinder mantle, the inner surface of which is made smooth. On the outer side of the cylinder, at least one channel is built in, which extends in the form of a [screw line] helix in the longitudinal direction of the cylinder and can be connected for conducting a tempering medium [that can flow]. In [contrast to the overall] the state of the art, [in which] the channel [in the form of a screw line] formed as a helix is closed in the radial direction through a part of the cylinder by separately produced cylinder sections, while the corresponding connection in the other regions of the circumference are closed directly by the hollow-cylinder mantel[, in] . In contrast the channels in the cylinder constructed according to the invention[, it is envisioned that the channel(s)] is/are closed over the entire circumference by the hollow-cylinder mantle itself. Thus no components are needed that correspond to the cylinder sections from the overall state of the art. A significant cost reduction for the cylinder according to the invention results from the circumstance that the channel(s) for the tempering medium are generated by a winding vortex. This involves an especially simple manufacturing process that can be implemented by placing the piece under tension and generating channels with a completely uniform [screw-line]

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helical course, which is a great advantage for the flow-through of the tempering medium. The channel(s) thus have no sudden kinks or other flow obstacles.--

On page 7, amend the paragraph beginning on line 11 as follows:

--In principle, the cylinder can be provided with a single channel with a [screw-line] helical shape. In most cases, however, it will be appropriate, such as with multiple windings, to provide several channels next to one other. Advantageously, there will be three or four such channels running parallel to one another on the outside of the cylinder. The pitch of the channel(s) will generally be kept constant over the length of the cylinder. In individual cases, however, it may be reasonable to change this pitch, in order to affect the dwell time of the tempering medium in a particular section of the cylinder along its longitudinal axis. By selecting a large pitch, the tempering medium can be fed in the direction in which the extruder moves or even in the opposite direction, as needed.--

On page 8, amend the paragraphs beginning on lines 1 and 20 as follows:

--In many cases, [it is advantageous to provide] a rectangular shape may be provided for the channel(s). The depths of each channel in the radial direction, i.e. its cycle depth, [can] may remain constant over the circumference of the cylinder. The advantage is that the wall thickness of the extrusion space is likewise constant over the circumference and thus the flow patch through the wall of the extrusion space for the heat to be transported -- seen over the circumference -- likewise remains constant. In regard to the arrangement of the individual

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windings of the channel(s) of the cylinder, it has turned out to be appropriate, especially with channels with a rectangular cross-section and a uniform cycle depth, that the width of the channel(s)(measured in the longitudinal direction of the cylinder) be set at in the region of the 0.7 to 1.2 times the thickness of the bridges [of the] between channels. The bridges are dimensioned in such a way that they provide directly an adequate support for load transfer to the hollow-cylinder mantle, without special components such as are needed in the cylinder section according to DE-OS 2,061,700.--

--In [the] an embodiment of the present invention, a design of the channel(s) with various cycle depths is provided over the circumferences. In this case, the cycle depth is selected as small as possible in the regions where the original wall thickness of the cylinder, i.e. the thickness before the channels are made, is smallest. The greatest cycle depth is provided in the regions in which the original wall thickness is greatest. The transition between the largest and smallest cycle depths run completely smoothly and uniformly, because of the winding-vortex process envisioned for producing the channels. For a twin-screw extruder, a cylinder is recommended in which the largest cycle depth of the channel is about 3 to 5 times the smallest cycle depth, especially preferably about 4 times. In this case it may be appropriate to select something other than a rectangular shape and provide a conic expansion in the outward direction for the cross-section in the radial direction. The width of each channel thus increases in the outward direction. This means that the side surfaces of each channel in the section through the length of the cylinder do not run parallel, but include an angle,  $\alpha$ . This angle,  $\alpha$ , is advantageously in the range of 8-15°, especially about 10°. With a conic shape for the cross-

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section of the channels, it is recommended that the average thickness of the bridges between each pair of adjacent windings in the channel(s) be selected in the range of 1.5 to 4 times the average width of the channel(s). An average bridge width of about 2.5 times the average channel width is preferred.--

On page 10, amend the paragraph beginning on line 9 as follows:

--Beyond the low manufacturing costs, the cylinder according to the present invention provides an effective heat exchange, since through the effect of the cycle depth of the channels the flow path for the heat can be reduced within the wall of the cylinder as needed. Increased resistances to the flow of heat due to separation surfaces between individual components are avoided in the invention. For a given cylinder diameter, it makes no difference for the design of the hollow-cylinder mantle surrounding the cylinder how many channels, with which cross-section shape, and which cycle depths are provided in the cylinder.--

On page 10, delete lines 20-22 in their entirety and insert the following therefore:

**--BRIEF DESCRIPTION OF THE DRAWINGS**

In the drawings wherein like reference characters denote similar elements  
throughout several views:--

On page 11, amend the paragraph beginning on line 1 as follows:

-- Fig. 1 [shows] is a perspective view of a cylinder according to an embodiment of the invention[,] ;

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Fig. 2 [shows] is a view from the right front side of the cylinder according to Fig. 1[,] ;

Fig. 3 [shows] is a longitudinal section along line [A-A] III-III in Fig. 2[,] presenting a view of the upper half,] ;

Fig. 4 [shows] is a longitudinal section along line [B-B] IV-IV in Fig. 2[,] presenting a view of the lower half,] ;

Fig. 5 [shows] is a cross-section along line [C-C] V-V in Fig. 3[,] ;

Fig. 6 [shows] is a view of the left front side of the cylinder according to Fig. 1[,] ; and

Fig. 7 [shows] is the cylinder according to Fig. 1 inserted into a cylindrical mantle in a partial side view and partial longitudinal section.--

On page 11, after line 14, beginning its own line, insert the following heading:

**--DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT--**

On page 11, amend the paragraph beginning on line 15 as follows:

-- [The] A cylinder 1 shown in perspective in Fig. 1 is provided for an extruder with a twin-screw unit and therefore has two partially overlapping holes for the two meshed screws (not shown), whereby the holes together form an extrusion space 2 with a cross-section in the shape of spectacles. [In] An application flange 14 in the region of the [left] front side of the cylinder 1 (on the left side in Fig. 1), [an application flange 14 is provided, which, as can be seen especially in Figs. 3 and 4,] has a diameter that is only slighter larger than that of the [cylinder 1

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in the rest] remainder of [its] the length of the cylinder. On the outer side of the cylinder 1, a number of windings of channels 3 are provided in the shape of a [screw line] helix, between which bridges 4 stand as separation walls.--

On page 12, amend the paragraph beginning on line 2 as follows:

--The implementation of the channels 3 can be seen in detail from the section views of Figs. 3 through 5. The axial longitudinal section in Fig. 3 [along line A-A according to Fig. 2] shows that the channels 3 each have side walls 5, 6 that are at an angle[,]  $\alpha$ [,] to each other, so that the channel [cross-section] width expands conically outward in the radial direction. The average width of the bridges 4 between the individual windings of the channels 3 is about 2 to 2½ times the average width of the channels 3(measured in the longitudinal direction of the cylinder 1). It can be seen from [the cross-section made along line C-C according to Fig. 3, which is shown in] Fig. 5[,] that a total of four channels are involved here, which extend at equal distances from each other in [the] a helical shape [of a screw line] over the [essential part of] the axial length of the cylinder 1. It can also be seen from Fig. 5 that the cycle depth of the channels 3, i.e. [their] the radial depth [in the radial direction of the cylinder 1], is not constant over the course of the circumference of the cylinder 1, but changes uniformly in the region near the planes through the longitudinal axis of the extrusion space 2, in which the cycle depth in the channels 3, indicated by  $h_2$ , is the greatest. The uniform change of the cycle depth between the largest value,  $h_2$ , and the smallest value,  $h_1$ , results in a simple manner from a corresponding setting of the process parameters used in the winding vortex process used in producing the channels 3. Whereas Fig. 3 shows a side view and a longitudinal cross-section in the region of

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the smallest cycle depth,  $h_2$ , in Fig. 4 a longitudinal section [along line B-B] is shown, rotated by 90° i.e., in the region of the smallest cycle depth. By varying the cycle depth over the circumference of the cylinder 1, [it is achieved that] extreme differences in heat flow between the extrusion space 2 and the channels 3 over the circumference of the cylinder 1 are greatly reduced. Each of the four channels 3 opens into a groove 7, [or] 8 that respectively runs around and near to the [front] end of the cylinder 1[, which has the function of]. The grooves 7, 8 act as a distributor [or] and a collector for the tempering fluid to be fed through the channels 3.--

On page 13, amend the paragraph beginning on line 15 as follows:

--In Fig. 6, a view of the front side of the cylinder 1 is shown with the application flange 14. As can also be seen in Fig. 2, holes to accept adjusting bolts 15 are provided in the region of the greatest wall thickness[, which] (The adjusting bolts are shown in detail in the side view of Fig. 7). [Fig. 7 shows the structure of a] A complete cylinder assembly 11, consisting of the cylinder 1 and the associated hollow-cylinder mantel 10, in halves in the longitudinal section , is shown in Fig. 7 . The hollow-cylinder mantle 10, which has connecting flanges 17, 18 on each of its two ends, [is made] has a smooth [on its] inner surface. Only in the region of the application flange 14 does it have a section with an enlarged inner diameter, which corresponds to the outer diameter of the application flange 14 of the cylinder 1, so that the application flange 14 can be applied in this section and be held as a stop against shifts by the cylinder 1 in the longitudinal direction. The inner diameter of the hollow-cylinder mantle 10 corresponds to the outer diameter of the bridges 4 of the cylinder 1, which is thus embedded as a "moist bushing" in the hollow-cylinder mantle 10, so that the individual windings of the channels 3 are closed in the

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radial direction toward the outside. There is a radial hole through the connection surfaces 17, 18 for feeding the intake 12 and the outlet 13 of the tempering medium, which end in the region of the circumferential grooves 7, 8. The connection between the circumferential groove 8 and the outlet 13 is not as direct as between the circumferential groove 7 and the intake 12. Rather, the connection is made in this case through an indentation 19 in the application flange 14. The tempering medium can thus flow through the intake 12 in the circumferential groove 7, which functions as a distributor, and from there into the four channels 3 in the shape of a screw line. After flowing through the channels 3, the tempering medium arrives at the circumferential channel 8, which functions as a collector and is there again removed through the indentation 19 and the line 13 from the full cylinder assembly 11. During the flow through the channels 3, an effective heat exchange takes place between the tempering medium and the extrusion space 2.--

On page 15, amend the paragraph beginning on line 2 as follows:

--[Because] To prevent the cylinder 1 [cannot be turned] from turning with respect to the hollow-cylinder mantle 11, stop grooves 9 are provided in the region of the circumference of the application flange 14, into which pin screws 16 make contact through corresponding holes made radially through the connection flange 18. Through the connection flanges 17, 18, several full [cylinders] cylinder assemblies 11 can be connected together. In this case it is obviously possible, with a hollow-cylinder mantle 10 of unchanged construction with respect to the channels, to use various cylinders 1, in order to meet optimally the different needs for heat exchange (cooling or heating) along the extrusion space.--

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In the Abstract:

Please amend the Abstract as follows:

--[The invention concerns a] A cylinder assembly for a twin-screw extruder[, where] includes a cylinder [the cylinder (1) surrounds a twin screw of the extruder,] forming an extrusion space [(2)] and [is in turn surrounded by] a hollow-cylinder mantle surrounding the cylinder [(10), which has] and having a smooth inner surface[,] . [where on the outside of the cylinder (1) at] At least one channel [(3)] is made in the shape of a [screw line] helix in the longitudinal direction on the outside of the cylinder [(1).] . [which can be] The at least one channel is connected to an intake and outlet [(12, 13)] for conducting a tempering medium [that is capable of flowing, and can be closed, at least over part of the circumference of the cylinder (1), in the radial direction by the hollow-cylinder mantle (10). In this case,] The at least one channel [(3)] is made [in the cylinder (1)] by a winding-vortex process and the at least one channel[(s) (3) [are]] is closed by the hollow-cylinder mantle [(10)]. The cycle depth of the at least one channel[(s) (3)] in the radial direction changes over the circumference of the cylinder [(1) in] such [a way] that it is greatest in regions where the original wall thickness of the cylinder [(1)] is greatest, and that it is smallest in the regions where the original wall thickness of the cylinder [(1)] is also smallest.

[Figure 1 attached.]